

**An Investigation of Deterministic and Stochastic Properties of
Microwave/Millimeter Wave Signals Generated in
Laser Diodes with Short External Cavity**

Final Report

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1. Introduction

Future military analog fiber-optic links require high-bandwidth (20-30 GHz) and large dynamic range (>120 dB) that are, furthermore, compact, light weight, and with low power consumption. Technologies that have been investigated so far can not meet the above-mentioned demands. These technologies include, cw laser diode direct modulation, mode-locked laser diode external modulation, and external modulation.

Optical coupling of a Laser diode (LD) with an external cavity (EC), such as shown schematically in Fig. 1, has been used to improve laser frequency stability and to narrow laser linewidth. Such coupling can also significantly change LD dynamics. For long (>1 cm) external cavity LDs these changes lead to chaotic self-modulation of laser light with dramatic broadening of laser spectrum ("coherence-collapse" effect). For a short EC LD there exists another type of instability associated with the EC mode interactions alone [1]. The compound-cavity mode interaction inside the regime of stable CW operation lead to the generation of high frequency (>20 GHz) microwave oscillations. Such high-frequency oscillations arise, as has been conjectured [1], if the cavity losses for the main and side compound-cavity modes of the short EC LD become equal with increasing feedback. This equalization does not lead, however, to a switching of lasing to this sidemode, but instead induces a self-mode-locking regime with deep oscillations of the laser output.

We propose to use short EC LDs as tunable microwave oscillators with frequency modulation capabilities. There are two ways the frequency can be modulated [2].

- It has been shown that the oscillation frequency increases with increasing feedback. Therefore, the frequency of the microwave oscillation can be modulated by the feedback
- It should be noted that the oscillation is a result of the interaction of compound-cavity mode interaction. Therefore, once the optical length of the individual cavity is changed, the oscillation is tuned.

We have previously computed the dynamics of short EC LDs, mapped out the system parameter space for microwave oscillations, and determined the frequency range of the microwave oscillations.

The ultimate research objective is to *experimentally* demonstrate the generation of tunable microwave intensity oscillations in laser diodes with short external cavity for use in analog fiber-optic links. A better understanding of the fundamental mechanism is therefore essential for progress towards employing these devices in real applications. In this report, we document enhanced understanding of the underlying physical principle for the microwave-frequency intensity modulation from a nonlinear dynamics point of view, and ways to experimentally measure the noise characteristics of the oscillations.

2. Investigation of the Noise Characteristics

2.1 Preliminary Comment

Periodic orbits in nonlinear optical systems, such as the high-frequency oscillations described in Sections 2 and 3 can serve as subcarriers in optical communications. Subcarrier optical communication using one form of periodic orbits commonly known as self-sustained pulsations (SSP) [5] has been experimentally demonstrated both for analog [6] and digital [7] applications. The signal-to-noise ratio (bit-error-rate) of the analog (digital) subcarrier systems depends on the nature and magnitude of the noise of the subcarrier. Since only one harmonic in SSP is used as the subcarrier, the amplitude and phase noise of each harmonic in SSP needs to be characterized. In this report we report the first, to the best of our knowledge, calibrated measurement of amplitude and phase noise of self-pulsations in two-section Fabry-Perot laser diodes (LDs).

2.2 Experimental Setup

Figure 1 illustrates the experimental setup for the measurement of amplitude and phase noise of SSP in commercially available 780 nm SSP LDs. The SSP is first converted into RF signals with a high-speed photodetector (3 dB bandwidth >14 GHz). The RF spectrum of SSP is monitored using a broadband RF spectrum analyzer (HP 8565E). By using bandpass filters, individual harmonic of the RF signal can be selected for amplitude and phase noise measurement using the HP 3048A Noise Measurement

System, which is a calibrated measurement system dedicated for RF/microwave oscillator noise characterization for frequency offsets as small as 1 Hz.

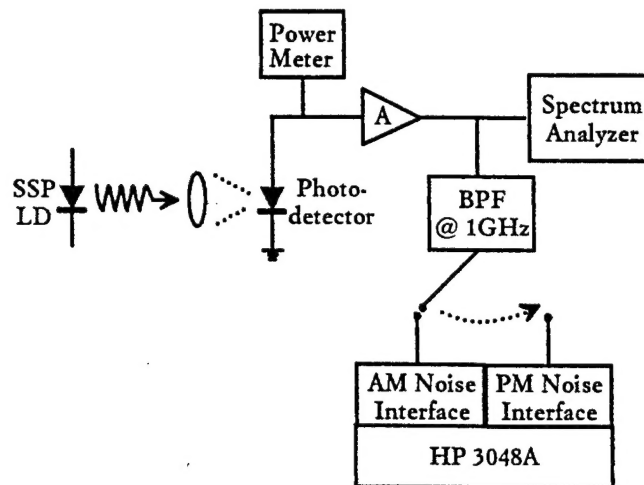


Figure. 1 Experimental setup for the amplitude and phase noise measurement

2.3 Results

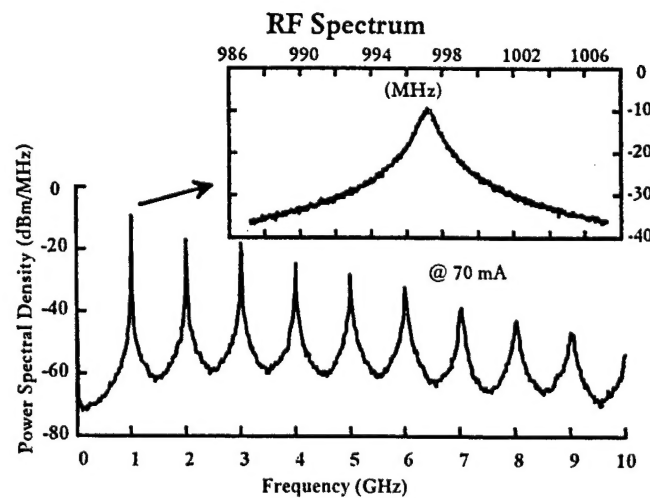


Figure. 2 RF spectrum of SSP with a 1 GHz fundamental frequency in a laser diode.

A typical RF spectrum of SSP is shown in figure 2. At 70 mA DC bias current, the SSP frequency is around 1 GHz (The threshold is at 50 mA). More than 15 harmonics can be observed. Each harmonic has a certain linewidth which increases with its order. Details around the fundamental harmonic, given in the inset, reveals a 3-dB linewidth on the order of 1 MHz. Because the fundamental harmonic was used in previous experiments [6,7] and because of the instrumentation frequency limitations, we focused on the noise characterization of the fundamental harmonic in the present effort. With a 1 GHz bandpass filter of 400 MHz bandwidth, the amplitude and phase noise of fundamental harmonic are investigated nearly independent of each.

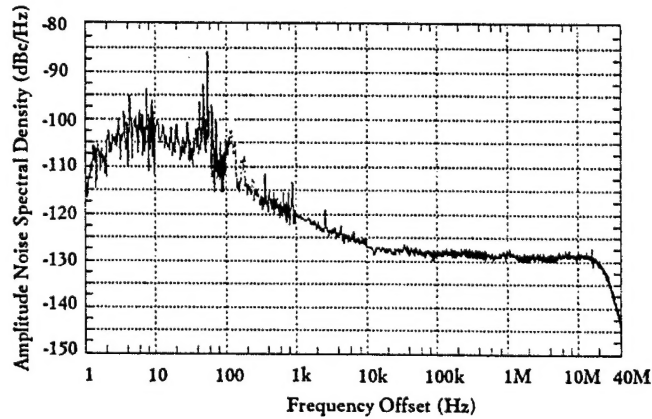


Figure. 3 Amplitude noise spectrum of the fundamental harmonic.

The amplitude noise is measured first because the AM noise interface offers a better than 110-dB discrimination against phase noise. The amplitude noise spectral density in dBc, which represents the AM noise sideband to carrier power ratio, is given in figure 3. Comparing the RF and AM noise spectra, it is apparent that amplitude noise

has a negligible contribution to the overall noise power leading to the 1 MHz linewidth. Therefore, the noise of the fundamental harmonic has to be primarily phase noise. The phase noise interface is essentially a delay-line frequency discriminator, which measures the noise frequency deviation from the center frequency due to phase noise. Figure 4 shows the phase noise spectrum of the fundamental harmonic for 1 Hz to 40 MHz frequency offset from the center frequency of the carrier. Below 1 kHz offset, the noise frequency deviation is $1/f$ in nature. The peak around 60 Hz results from the power supply. For the frequency offsets above 10 kHz, frequency deviation noise is white with a magnitude of around $600 \text{ Hz} / \sqrt{\text{Hz}}$. The decrease near 40 MHz offsets is due to the bandwidth limitation of the HP 3048A system. Assuming a $600 \text{ Hz} / \sqrt{\text{Hz}}$ pure frequency fluctuation which is white in nature, the theoretically [8] estimated carrier linewidth is about 1.13 MHz which matches very well with the observed RF spectrum.

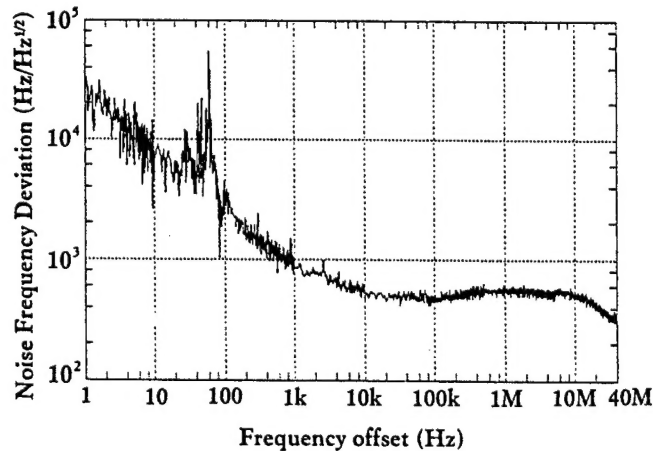


Figure. 4 Phase noise spectrum of the fundamental harmonic

2.4 Summary

We have investigated experimentally the noise behavior of self-sustained pulsation in laser diodes. Frequency deviation and amplitude fluctuation of the pulsation have been characterized in the range of 1 Hz to 40 MHz. Even though phase noise dominates over amplitude noise, both are $1/f$ in nature for offsets below 1 kHz, and white for offsets above 10 kHz. This technique can be applied to the noise measurement of the high-frequency oscillation in ECLDs also.. In addition to understanding and ultimately improving the performance of periodic-orbit subcarrier optical communication systems, further research along this line will be useful for other applications such as all-optical clock recovery [9].

3. Investigation of Deterministic Properties: Formulation

3.1 Rate Equation

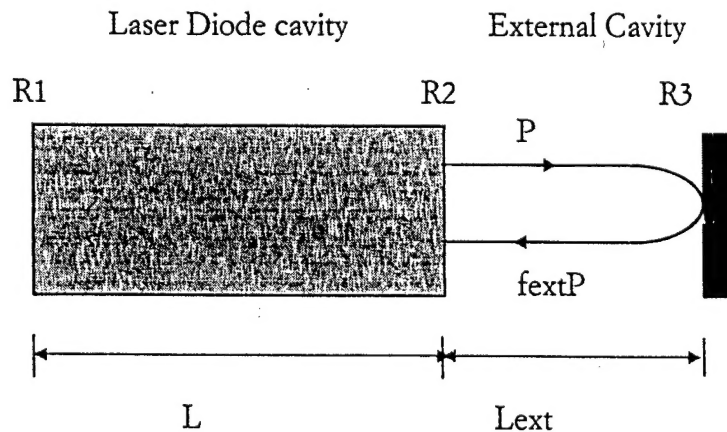


Fig. 5 Schematic of a laser diode with an external cavity.

The schematic of a semiconductor laser diode with an external cavity is shown in Fig. 1. R_1 and R_2 are the reflectivity of the laser facets and R_3 is the reflectivity of the external mirror. L and L_{ext} are the lengths of the laser diode cavity and the EC; f_{ext} is the feedback. We will consider $\tau\omega_R \ll 1$, where $\tau = 2L_{ext}/c$ is the photon round-trip time in EC and ω_R is the angular frequency of the relaxation oscillation.

We adopt the Lang and Kobayashi rate equations for the SEC LD. There are several assumptions for these rate equations. First, the solitary laser is assumed to be single mode, which implies $\tau \gg \tau_0$ ($\tau_0 = 2Ln_g/c$, is the photon round-trip time in the LD-cavity, n_g is the group refraction index of the LD.). Second, $f_{ext} \ll 1$ which means only one round-trip of the emitted photons is significant inside the EC. Then we arrive at the following two rate equations :

$$\frac{dE(t)}{dt} = j \left[\Omega_s - \Omega + \frac{\alpha}{2} g_N (N - N_s) \right] E(t) + \frac{1}{2} \left(g - \frac{1}{\tau_p} \right) E(t) + \kappa E(t - \tau) \exp(-i\Omega\tau) \quad (1)$$

$$\frac{dN}{dt} = J - \frac{N}{\tau_{sp}} - gS \quad (2)$$

where $g = g(N)(1 - \kappa_p P)$ is the nonlinear gain where the differential gain is given by $g(N) = g_N(N - N_s)$, P is the output power, Ω_s is the resonance optical frequency of the LD without EC, α is the linewidth enhancement factor, g_N is the differential gain, τ_p is the photon lifetime in the LD cavity, τ_{sp} is the carrier lifetime due to spontaneous

and nonradiative recombination, $S = |E(t)|^2$ is the photon number in the LD cavity.

(output power $P \sim S$), J is the carrier injection rate. The feedback parameter is given by

$$\kappa = \frac{C_l}{\tau_0},$$

where parameter C_l which is a function of the facet and external mirror reflectivity R_2 and R_3

$$C_l = (1 - R_2) \sqrt{\frac{R_3}{R_2}}$$

is a measure of the coupling strength between the two cavities. The rate equations for the EC LD are given in equations (1) and (2). The absolute squared value of the electric field amplitude corresponds to the number of photons in the laser cavity. Equations (1) and (2) can be cast into rate equations for the photon number S , the phase ϕ , and the carrier number N :

$$\frac{dS(t)}{dt} = \left(g - \frac{1}{\tau_p}\right)S(t) + 2\kappa\sqrt{S(t)}\sqrt{S(t-\tau)}\cos(\Omega_s\tau + \phi(t) - \phi(t-\tau)) \quad (3)$$

$$\frac{d\phi(t)}{dt} = \frac{\alpha}{2}g_N(N - N_s) - \kappa\frac{\sqrt{S(t-\tau)}}{\sqrt{S(t)}}\sin(\Omega_s\tau + \phi(t) - \phi(t-\tau)) \quad (4)$$

$$\frac{dN(t)}{dt} = J - \frac{N(t)}{\tau_{sp}} - gS(t) \quad (5)$$

3.2 Numerical Simulations

In numerical simulations, the system of rate equations system (3)-(5) is solved by using a fifth-order Runge-Kutta method [3],[4]. We specify the initial conditions

$S(0)=10$, $\phi(0)=0$ and $N(0)=0$. In the time interval $0 \leq t \leq \tau$, the data of photon number S and phase ϕ are stored in memory and they are reused after the round-trip time τ of the EC in order to account for the optical feedback.

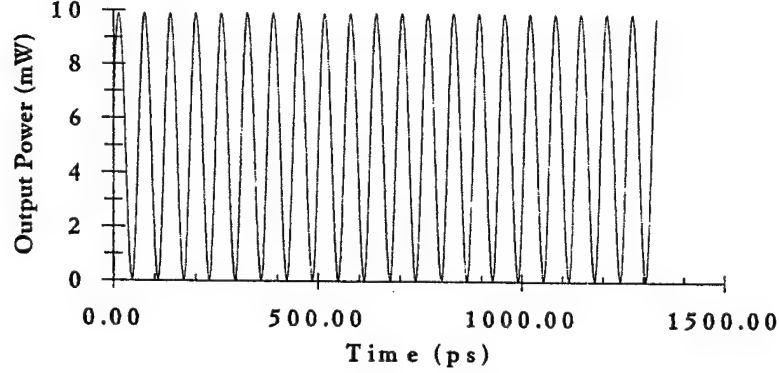


Fig. 6 The strongest oscillation for the $L_{ext}=5.25\text{mm}$ and the f_{ext} group. The feedback parameter is 0.206. The oscillation frequency is equal to 21.3 GHz.

3.3 An Example of High-Frequency Microwave Oscillation

For example, we set the output power $P=5$ mW/per facet. The calculations used the laser parameters given in Table I. Here, we also choose the EC length $L_{ext}=5.25$ mm. We found that the feedback parameters for the strongest modulation index occurs when $f_{ext}=0.206$. Further increasing f_{ext} destroys the twin mode locking. It leads the laser operation on a new single-mode state with higher output power (7.06 mW). The strongest oscillation frequency we get in the group f_{ext} is 21.3 GHz as shown in Fig. 2.

TABLE I
List of Parameters for Fabry-Perot laser

Parameter	Symbol	Value	Units
scattering loss in the active region	α_s	3.6×10^3	m^{-1}
carrier number at transparency	N_s	2.0×10^8	
output power	P	$2.906 \times 10^{-8} \times S$	$mW / facet$
index of active region	n_g	4.5	
differential gain	g_N	2.2×10^3	s^{-1}
linewidth enhancement factor	α	4	
laser wavelength	λ	.3	μm
spontaneous emission lifetime	τ_s	2.0×10^{-9}	s
photon lifetime	τ_p	$.29072 \times 10^{-12}$	s
gain saturation coefficient	k_p	4.8	W^{-1}

4. Investigation of Deterministic Properties: Bifurcation Analysis

Since the problem is nonlinear in nature, there does not exist a general analytical methodology that can lead to a global conclusion of the operation characteristics of the ECLD. Our approach is to establish a numerical technique that is capable of predicting the nature of the ECLD output given a complete set of parameters for the ECLD without numerical integration described in Section 2. We used a public-domain software called AUTO to investigate the dynamics of laser diodes with short external cavity. AUTO was developed in the Applied Mathematics Department at the California Institute of Technology as one of the projects of the Differential Equations Group in the Center for Research on Parallel Computation. In what follows, we describe the interface FORTRAN code for AUTO to simulate the laser diodes with external cavity and some

representative results. We stress that the results shown here only apply to the particular parameters chosen as indicated. To find the dynamic behavior of ECLDs with different parameters, one needs to run the AUTO program with the interface FORTRAN code with the modified ECLD parameters.

4.1 Bifurcation Diagrams of ECLD Steady States

To construct the bifurcation diagrams of ECLD steady states, the first step is to find all ECLD steady states for a given set of the ECLD parameters and then using AUTO to finding the continuations of the steady states.

To find all ECLD steady states for a given set of the ECLD parameters, a program such as “SEARCH_SS” can be used. SEARCH_SS finds all the solutions to the nonlinear algebraic equations:

$$(g - \frac{1}{\tau_p})S(t) + 2\kappa\sqrt{S(t)}\sqrt{S(t-\tau)}\cos(\Omega_s\tau + \phi(t) - \phi(t-\tau)) = 0 \quad (6)$$

$$J - \frac{N(t)}{\tau_{sp}} - gS(t) = 0 \quad (7)$$

arrived by setting the right-hand side of Eqs. (3) and (5) to be equal to zero. The program “SEARCH_SS” is given in Appendix 1..

Once all the steady states of the ECLD for the given set of parameters are found, the bifurcation diagram can be constructed by continuing the steady states as one of the

parameters in the parameter set is varied in both directions (increasing or decreasing). The interface FORTRAN code for this continuation is contained in Appendix 2. It is found that Hopf bifurcation delineates stable and unstable steady states.

4.2 Stability Boundaries of ECLD Modes

To construct the Stability-Boundary diagram of ECLD steady states, the first step is to find the Hopf bifurcation points of all ECLD steady states for a given set of the ECLD parameters and then using AUTO to finding the continuations of the Hopf bifurcation points.

To find Hopf bifurcation points of all ECLD steady states for a given set of the ECLD parameters, a program such as "SEARCH_ST" can be used. SEARCH_ST finds all the solutions to the nonlinear algebraic equations (6), (7), and (8)

$$D(s) = -s^3 + s^2[\gamma + 2\kappa e(\tau) \cos \phi] - s[\omega_R^2 + \kappa^2 e^2(\tau) + 2\gamma_e \kappa e(\tau) \cos \phi] + \kappa[\omega_R^2 e(\tau)(\cos \phi - \alpha \sin \phi) + \gamma_e \kappa e^2(\tau) + \alpha \gamma_e \gamma_p e(\tau) \sin \phi] \quad (8)$$

where $e(\tau) = 1 - e^{i\omega\tau}$ and $\phi = \Omega\tau$. Here $\gamma_e = 1/\tau_s + g_N S$ is the carrier perturbation decay rate, $\gamma = \gamma_e + \gamma_p$ is the decay rate of relaxation oscillations, with $\gamma_p = g\kappa_p P$ being the contribution of the nonlinear gain. The angular frequency of relaxation oscillations ω_R is given by $\omega_R^2 = gg_N S + \gamma_e \gamma_p$. Equation (8) is arrived by setting the determinant of the linearized ECLD system to be equal to zero. The program "SEARCH_SS" is given in Appendix 3.

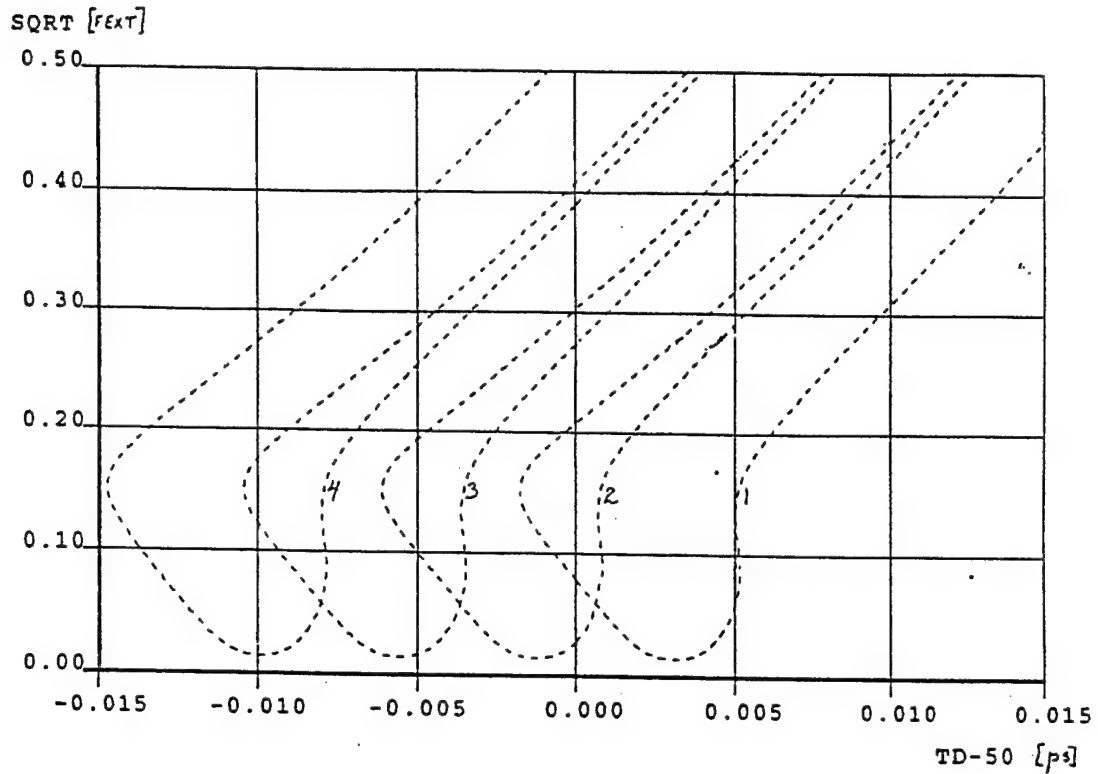


Fig. 7 The stability boundaries of 4 ECLD modes in the $\sqrt{f_{ext}} - \tau_d$ plane. The injection current is at twice the threshold.

Once Hopf bifurcation points of all the steady states of the ECLD for the given set of parameters are found, the bifurcation diagram can be constructed by continuing the steady states when one of the parameters in the parameter set is varied in both directions (increasing or decreasing). The interface FORTRAN code for this continuation is contained in Appendix 4.

4.3 Regions of Existence of ECLD Modes

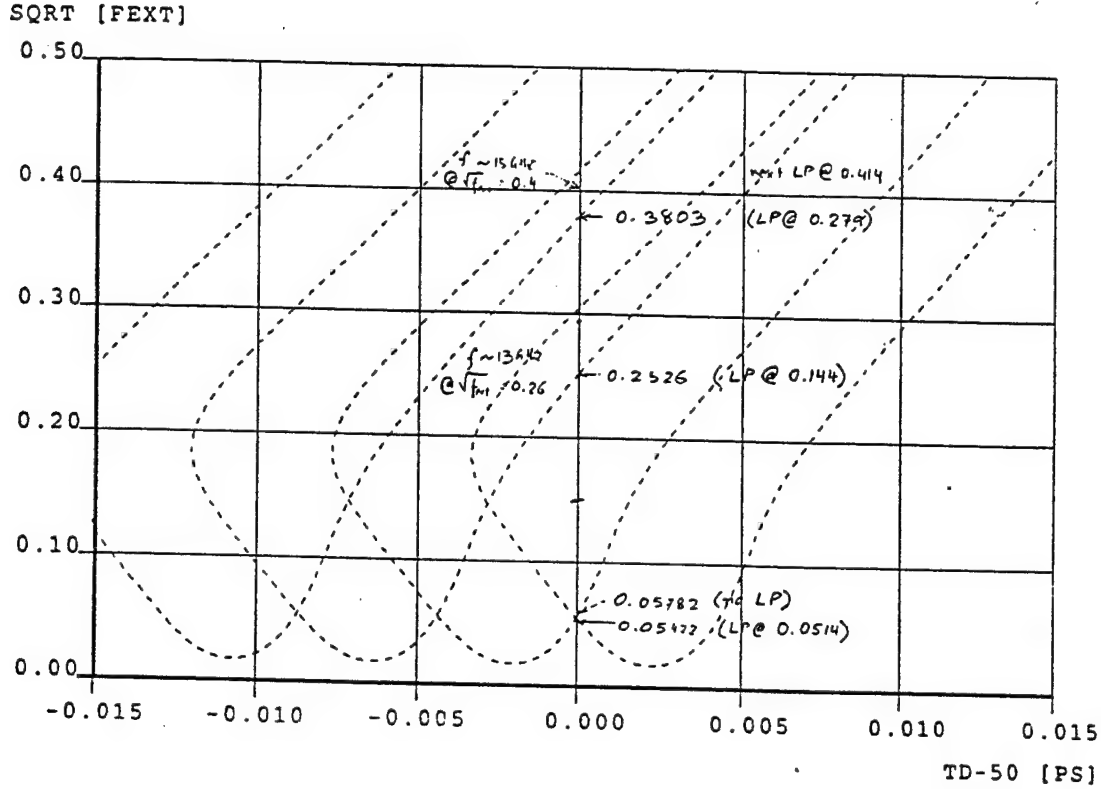


Fig. 8 Limiting points (LP) of existence of modes superimposed on the stability boundaries. When LP of a higher-order mode is above the stability boundary, robust high-frequency oscillations result. Parameters are the same as in Fig. 3, except that injection is three time the threshold.

It is found by numerical simulation that even in regions above the stability boundary of a particular, the high-frequency oscillations are not always present. We believe that this due to the existence of other modes, which might be stable in the unstable region of the mode that we are interested in. To do so, we calculated the regions of existence of all modes. High-frequency oscillations are produced only if the

boundary of existence [limiting point (LP) of existence] of higher-order modes is above the stability boundary. An example where robust high-frequency oscillation are possible is shown below.

4.4 Investigation of Deterministic Properties: Experiments

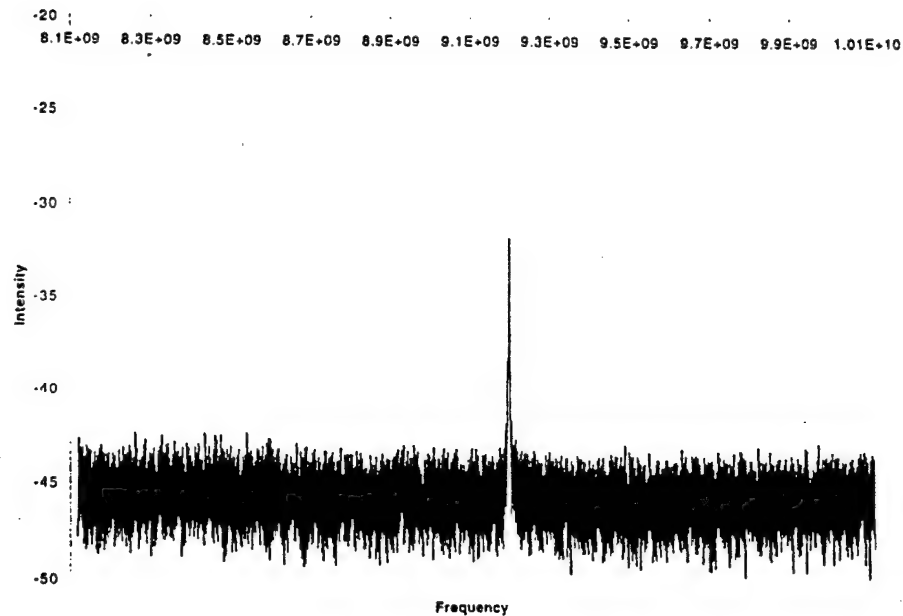


Fig. 9 RF spectrum of a 9.2 GHz subcarrier generated in ECLD.

Using a Fabry-Perot laser diode and an optical flat as the external mirror, The high-frequency intensity oscillations have been generated. The highest frequency achieved is 9.5 GHz, as shown in Fig. 9. Modulation of these oscillations has also been demonstrated. Up to 750 MHz modulation has demonstrated. The modulated signal,

shown in Fig. 10 reveals excellent frequency modulation characteristics with minimal residual amplitude modulation, as the two sidebands are almost equal in strength.

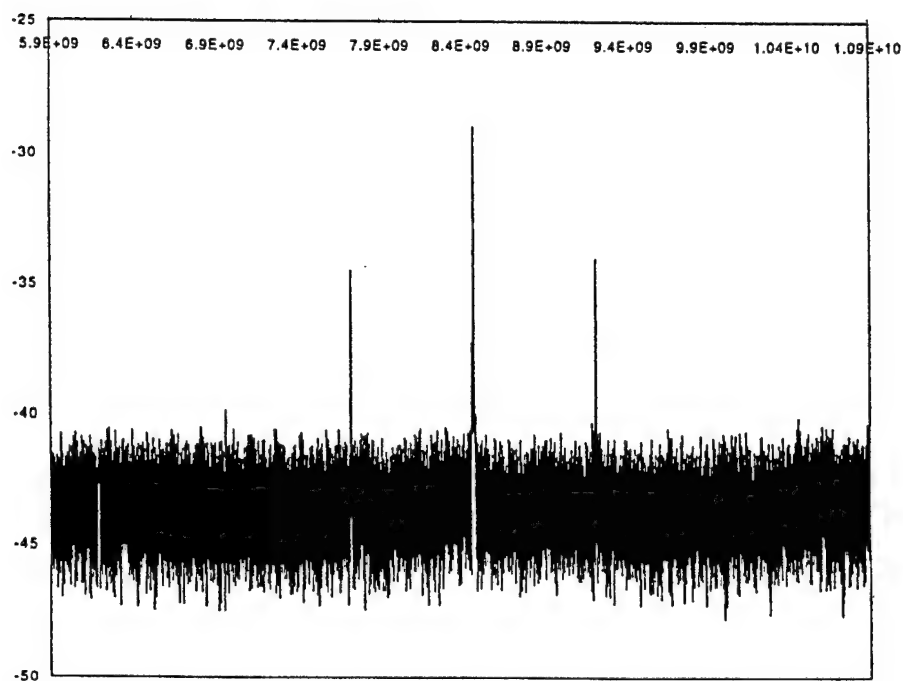


Fig. 10 RF spectrum of a 8.4 GHz subcarrier modulated by a 750 MHz signal.

5. Conclusions

In conclusion, we have determined the underlying mechanism of the high-frequency intensity oscillations in laser diodes with short external cavity. From a nonlinear dynamic point of view, Hopf bifurcation is responsible for the occurrence of the high-frequency intensity oscillations. However, Hopf bifurcation is only the necessary condition. The necessary and sufficient condition are that Hopf bifurcation occurs and the limiting point of existence of a higher-order mode is above the stability boundary of a lower-order mode. The noise characteristics of the high-frequency oscillations can be measured using the HP 3048A phase and amplitude noise measurement system.

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Appendix 1

```
PROGRAM SEARCH_SS
C -----
C
C      Search for steady states of the external cavity laser diode
(ECLD).
C
C      Program based on algorithm 554 (routine BRENTM) of TOMS.
C
C      IMPLICIT REAL*8 (A-H,O-Z)
      DIMENSION X(10),FVEC(10),WA(130)
      EXTERNAL FUNC
      COMMON /ECLD/ GN,TP,EP,R,T0,FEXT,TD,ALP,W0,TS,RJTH,RJ,WOT
      COMMON /SEARCH/ ISEED,NSF,XF(100,10),PAR(10)
C
C      Get ECLD parameters and store in common block ECLD
C
      CALL GETPAR
C
C      The C parameter. For C >> 1, the number of steady states is
      approximately C/PI+1.
C
      WRITE (*,100) (1.0-R)*DSQRT(FEXT/R)*TD/T0
C
      OPEN  (1,FILE='search_ss.out',STATUS='UNKNOWN')
      WRITE (1,*) ' '
      CLOSE (1)
C
      N = 2           !number of equations
      LWA = 130       !size of array WA (must be at least N*(N+3))
C
      WRITE (*,*) 'Enter TOL,NTRY (1.0E-15,1000 typical):'
      READ  (*,*)  TOL,NTRY
C
      ISEED = 1       !seed for random number generator in START
      NSF = 0         !number of solutions found
      DO 10 I = 1,NTRY
C
C          Generate trial starting values.
C
          CALL START(N,X)
C
C          Attempt to locate a root.
C
          CALL BRENT1(FUNC,N,X,FVEC,TOL,INFO,WA,LWA)
C
C          If current search is successfull, update library of solutions.
C
          IF (INFO.LE.3.AND.INFO.NE.0) CALL UPDATE(N,X,INFO)
C
      10 CONTINUE
C
C      Store and write roots in ascending order.
C
      CALL PIKSRT(NSF,XF(1,1),XF(1,2))
      OPEN  (1,FILE='search_ss.out',STATUS='UNKNOWN')
      DO 20 I = 1,NSF
C
```

```

C      Determine if the current solution is a mode or antimode
C
      ET = (1.0-R)*DSQRT(FEXT/R)*TD/T0
      DW = 1.0+ET*DSQRT(1.0+ALP**2)*DCOS(XF(I,1)+DATAN(ALP))
C
      WRITE (1,200) XF(I,1),XF(I,2),DW/DABS(DW)
20 CONTINUE
      CLOSE (1)
C
100 FORMAT ('C =',E11.4)
200 FORMAT (10E16.8)
C
      STOP
      END
C
      SUBROUTINE GETPAR
C      -----
C
C      Get ECLD parameters and store in common block ECLD.
C
      IMPLICIT REAL*8 (A-H,O-Z)
      COMMON /ECLD/ GN,TP,EP,R,T0,FEXT,TD,ALP,W0,TS,RJTH,RJ,WOT
C
      OPEN (1,FILE='ecl.d.in',STATUS='OLD')
      READ (1,*) GN !gain coefficient (8.1E-19 cm**3/ps)
      READ (1,*) TP !photon lifetime (2 ps)
      READ (1,*) EP !nonlinear gain coefficient (9.0E-18 cm**3)
      READ (1,*) R !laser facet reflectivity (0.31)
      READ (1,*) T0 !solitary laser cavity round trip time (8 ps)
      READ (1,*) FEXT !feedback fraction (1.0E-04)
      READ (1,*) TD !delay in external cavity (20ps for 3mm EC)
      READ (1,*) ALP !linewidth enhancement factor (6)
      READ (1,*) W0 !freq of solitary laser (1.45E+03 rad/ps for
WL=1300 nm)
      READ (1,*) TS !carrier lifetime (2ns)
      READ (1,*) RJTH !current density at threshold (8.55E+14 cm**3/ps)
      READ (1,*) RJ !current density relative to threshold (1.2)
      CLOSE (1)
C
      WOT = W0*TD-DMOD(W0*TD,8.0D0*DATAN(1.0D0))
      FEXT = FEXT**2
C
      RETURN
      END
C
      SUBROUTINE FUNC(N,X,F,M)
C      -----
C
C      Solve for steady state frequency of the external cavity laser
C      diode (ECLD). See Ritter and Haug, JOSA B, Vol. 10, p. 130, 1993.
C
C      X(1) = W*TD
C      X(2) = ES/E0
C
C      M is the component of F to be returned, N is the number of
C      equations
C      and X is an N-vector containing values of the independent
C      variables.
C
      IMPLICIT REAL*8 (A-H,O-Z)

```



```

      DIMENSION X(N),F(N)
      COMMON /ECLD/ GN,TP,EP,R,TO,FEXT,TD,ALP,W0,TS,RJTH,RJ,WOT
C
      ET = (1.0-R)*DSQRT(FEXT/R)*TD/TO
      E0 = TP*(RJ-1.0)*RJTH
      GS = 1.0/TP-2.0*ET/TD*DCOS(X(1))
      DN = (GS/(1.0-EP*X(2)*E0)-1.0/TP)/GN
C
      F(1) = X(1)-(W0*TD-WOT)-ALP*GN*DN*TD/2.0+ET*DSIN(X(1))
      F(2) = GS*X(2)*E0-(RJ-1.0)*RJTH+DN/TS
C
      RETURN
      END
C
      SUBROUTINE START(N,X)
C
C
C
C      Generate random starting values for X. N is the number of
      equations.
C
      IMPLICIT REAL*8 (A-H,O-Z)
      COMMON /SEARCH/ ISEED,NSF,XF(100,10),PAR(10)
      DIMENSION X(N)
C
C      Generate a random number between X1L and X1H within which X(1) is
C      expected to lie. RAND is in the range (0,1).
C
      ISEED = MOD((2**10+3)*ISEED,2**20)
      RAND = DBLE(ISEED)/2**20
      X1L = -4.0D1*DATAN(1.0D0)
      X1H = 4.0D1*DATAN(1.0D0)
      X(1) = (X1H-X1L)*RAND+X1L
C
C      Generate another random number.
C
      ISEED = MOD((2**10+3)*ISEED,2**20)
      RAND = DBLE(ISEED)/2**20
      X1L = 0.0D0
      X1H = 2.0D0
      X(1) = (X1H-X1L)*RAND+X1L
      RETURN
      END
C
      SUBROUTINE UPDATE(N,X,INFO)
C
C
C
C      Update the library of solutions.
C
      IMPLICIT REAL*8 (A-H,O-Z)
      DIMENSION X(N),XOLD(10)
      COMMON /SEARCH/ ISEED,NSF,XF(100,10),PAR(10)
C
C      Check to see if the current data point already found earlier to
C      within a relative tolerance of 1.0E-07. If so, return.
C
      OPEN (1,FILE='search_ss.out',STATUS='OLD')
      REWIND 1
10  READ (1,100,END=30) (XOLD(I), I=1,N)
      DO 20 I = 1,N
          DIFF = DABS(XOLD(I)-X(I))
          IF (DIFF.GT.(1.0D-07*DABS(X(I)))) THEN

```

```

        IF (DABS(X(I)).GT.1.0D-10) GO TO 10
    ENDIF
20 CONTINUE
    CLOSE (1)
    RETURN
C
30 NSF = NSF+1
C
    DO 40 I = 1,N
        XF(NSF,I) = X(I)
    40 CONTINUE
C
    OPEN (1,FILE='search_ss.out',STATUS='OLD')
    WRITE (1,100) (X(I), I=1,N)
    CLOSE (1)
C
100 FORMAT(125E16.8)
C
    RETURN
    END
C
    SUBROUTINE PIKSRT (N,ARR,BRR)
    -----
C
C   Sorts an array ARR of length N into ascending numerical order, by
C   straight insertion, while making the corresponding rearrangement
of
C   the array BRR.
C
    IMPLICIT REAL*8 (A-H,O-Z)
    DIMENSION ARR(N),BRR(N)
C
    DO 30 J = 2,N
        A = ARR(J)
        B = BRR(J)
        DO 10 I = J-1,1,-1
            IF (ARR(I).LE.A) GO TO 20
            ARR(I+1) = ARR(I)
            BRR(I+1) = BRR(I)
10     CONTINUE
            I = 0
20     ARR(I+1) = A
            BRR(I+1) = B
30 CONTINUE
C
    RETURN
    END

```

Appendix 2

```

+++      SUBROUTINE FUNC(N,X,ICP,PAR,IJAC,F,DFDU,DFDP)
C      -----
C
C      Continuation of the steady state solution of the external cavity
C      laser diode (ECLD).
C
C      X(1)=WT, where WT is the steady state phase shift in external
cavity
C      X(2)=ES/E0, where ES and E0 are the steady state field
intensities of
C      the ECLD and the solitary laser, respectively.
C      PAR(1)=RJ, current density relative to threshold
C
IMPLICIT REAL*8 (A,B,D-H,O-Z)
      IMPLICIT COMPLEX*16 (C)
      DIMENSION X(N),F(N),PAR(*)
      COMMON /ECLD/ GN,TP,EP,R,TO,FEXT,TD,ALP,W0,TS,RJTH,RJ,WOT
C
C      Update ECLD parameters.
C
      RJ = PAR(1)
C
      ET = (1.0-R)*DSQRT(FEXT/R)*TD/TO
      E0 = TP*(RJ-1.0)*RJTH
      GS = 1.0/TP-2.0*ET/TD*DCOS(X(1))
      DN = (GS/(1.0-EP*X(2)*E0)-1.0/TP)/GN
C
      F(1) = X(1)-(W0*TD-WOT)-ALP*GN*DN*TD/2.0+ET*DSIN(X(1))
      F(2) = GS*X(2)*E0-(RJ-1.0)*RJTH+DN/TS
C
      RETURN
      END
C
      SUBROUTINE STPNT(NDIM,U,PAR)
C      -----
C
C      Starting conditions.
C
      IMPLICIT REAL*8 (A-H,O-Z)
      DIMENSION U(NDIM),PAR(*)
      COMMON /ECLD/ GN,TP,EP,R,TO,FEXT,TD,ALP,W0,TS,RJTH,RJ,WOT
C
C      Get ECLD parameters and store in common block ECLD
C
      CALL GETPAR
C
      OPEN (1,FILE='search_ss.out',STATUS='OLD')
      READ (1,*) (U(I), I=1,NDIM)
      CLOSE (1)
C
      PAR(1) = RJ
C
      RETURN
      END
C
      SUBROUTINE GETPAR
C      -----
C
      Get ECLD parameters and store in common block ECLD.

```

```

C
  IMPLICIT REAL*8 (A-H,O-Z)
  COMMON /ECLD/ GN,TP,EP,R,T0,FEXT,TD,ALP,W0,TS,RJTH,RJ,WOT
C
  OPEN (1,FILE='ecl.d.in',STATUS='OLD')
  READ (1,*) GN !gain coefficient (8.1E-19 cm**3/ps)
  READ (1,*) TP !photon lifetime (2 ps)
  READ (1,*) EP !nonlinear gain coefficient (9.0E-18 cm**3)
  READ (1,*) R !laser facet reflectivity (0.31)
  READ (1,*) T0 !solitary laser cavity round trip time (8 ps)
  READ (1,*) FEXT !feedback fraction (1.0E-04)
  READ (1,*) TD !delay in external cavity (20ps for 3mm EC)
  READ (1,*) ALP !linewidth enhancement factor (6)
  READ (1,*) W0 !freq of solitary laser (1.45E+15 rad/s for
WL=1300 nm)
  READ (1,*) TS !carrier lifetime (2ns)
  READ (1,*) RJTH !current density at threshold (8.55E+14 cm**3/ps)
  READ (1,*) RJ !current density relative to threshold (1.2)
  CLOSE (1)
C
  WOT = W0*TD-DMOD(W0*TD,8.0D0*DATAN(1.0D0))
  FEXT = FEXT**2
C
  RETURN
  END
C
  SUBROUTINE BCND
  -----
C
C
C  Dummy routine
C
  RETURN
  END
C
  SUBROUTINE ICND
  -----
C
C
C  Dummy routine
C
  RETURN
  END
C
  SUBROUTINE FOPT
  -----
C
C
C  Dummy routine
C
  RETURN
  END

```

```

      DW = 1.0+ET*DSQRT(1.0+ALP**2)*DCOS(XF(I,3)+DATAN(ALP))
C
      WRITE (1,100) XF(I,1),XF(I,2),XF(I,3),XF(I,4),DW/DABS(DW)
20 CONTINUE
      CLOSE (1)
C
100 FORMAT (11E16.8)
C
      STOP
      END
C
      SUBROUTINE GETPAR
C
C -----
C
C      Get ECLD parameters and store in common block ECLD.
C
      IMPLICIT REAL*8 (A-H,O-Z)
      COMMON /ECLD/ GN,TP,EP,R,T0,FEXT,TD,ALP,W0,TS,RJTH,RJ,WOT
C
      OPEN (1,FILE='ecl.d.in',STATUS='OLD')
      READ (1,*) GN      !gain coefficient (8.1E-19 cm**3/ps)
      READ (1,*) TP      !photon lifetime (2 ps)
      READ (1,*) EP      !nonlinear gain coefficient (9.0E-18 cm**3)
      READ (1,*) R        !laser facet reflectivity (0.31)
      READ (1,*) T0       !solitary laser cavity round trip time (8 ps)
      READ (1,*) FEXT     !feedback fraction (1.0E-04)
      READ (1,*) TD       !delay in external cavity (20ps for 3mm EC)
      READ (1,*) ALP      !linewidth enhancement factor (6)
      READ (1,*) W0       !freq of solitary laser (1.45E+15 rad/s for
WL=1300 nm)
      READ (1,*) TS       !carrier lifetime (2ns)
      READ (1,*) RJTH     !current density at threshold (8.55E+14 cm**3/ps)
      READ (1,*) RJ       !current density relative to threshold (1.2)
      CLOSE (1)
C
      WOT = W0*TD-DMOD(W0*TD,8.0D0*DATAN(1.0D0))
      FEXT = FEXT**2
C
      RETURN
      END
C
      SUBROUTINE FUNC(N,X,F,M)
C
C -----
C
C      Solve for steady state solutions and roots of determinant of
C      linearized rate equations of the external cavity laser diode
C      (ECLD).
C
C      X(1)=SQRT(FEXT), where FEXT is the feedback fraction
C      X(2)=W/2/PI, where W is the (circular) frequency of relaxation
C      oscil.
C      X(3)=WT, where WT is the steady state phase shift in external
C      cavity
C      X(4)=ES/E0, where ES and E0 are the steady state field
C      intensities of
C
C      the ECLD and the solitary laser, respectively.
C
C      M is the component of F to be returned, N is the number of
C      equations
C      and X is an N-vector containing values of the independent
C      variables.

```

Appendix 3

```

PROGRAM SEARCH_ST
C -----
C
C      Search for stability boundary of the external cavity laser diode
(ECLD).
C
C      Program based on algorithm 554 (routine BRENTM) of TOMS.
C
IMPLICIT REAL*8 (A-H,O-Z)
  DIMENSION X(10),FVEC(10),WA(130)
  EXTERNAL FUNC
  COMMON /ECLD/ GN,TP,EP,R,T0,FEXT,TD,ALP,W0,TS,RJTH,RJ,WOT
  COMMON /ECLDSS/ WS,ES,DN,GAMMAN,GAMMAI,GAMMA,OMEGSQ,ALPT
  COMMON /SEARCH/ ISEED,NSF,XF(500,10),PAR(10)
C
C      Get ECLD parameters and store in common block ECLD
C
  CALL GETPAR
C
  OPEN  (1,FILE='search_st.out',STATUS='UNKNOWN')
  WRITE (1,*) ' '
  CLOSE (1)
C
  N = 4           !number of equations
  LWA = 130       !size of array WA (must be at least N*(N+3))
C
  WRITE (*,*) 'Enter TOL,NTRY (1.0E-15,1000 typical):'
  READ  (*,*)  TOL,NTRY
C
  ISEED = 1       !seed for random number generator in START
  NSF = 0         !number of solutions found so far
  DO 10 I = 1,NTRY
C
C      Generate trial starting values.
C
    CALL START(N,X)
C
C      Attempt to locate a root.
C
    CALL BRENT1(FUNC,N,X,FVEC,TOL,INFO,WA,LWA)
C
C      If current search is successfull, update library of solutions.
C
    IF (INFO.LE.3.AND.INFO.NE.0) THEN
      IF (X(1).GT.0.0D0.AND.X(2).GT.1.0D-04.AND.X(4).GT.0.0D0
*      .AND.X(1).LT.0.5D0) CALL UPDATE(N,X,INFO)
    ENDIF
C
  10 CONTINUE
C
C      Sort and write roots in ascending order.
C
  CALL PIKSRT(NSF,XF(1,1),XF(1,2),XF(1,3),XF(1,4))
  OPEN  (1,FILE='search_st.out',STATUS='UNKNOWN')
  DO 20 I = 1,NSF
C
C      Determine if the current solution is a mode or antimode
C
    ET = (1.0-R)*XF(I,1)/DSQRT(R)*TD/T0

```

```

C      IMPLICIT REAL*8 (A,B,D-H,O-Z)
      IMPLICIT COMPLEX*16 (C)
      DIMENSION X(N),F(N)
      COMMON /ECLD/ GN,TP,EP,R,T0,FEXT,TD,ALP,W0,TS,RJTH,RJ,WOT
      COMMON /ECLDSS/ WS,ES,DN,GAMMAN,GAMMAI,GAMMA,OMEGSQ,ALPT
C
      FEXT = X(1)**2
C
C      Determine steady state parameters and store in common block ECLDSS
C
      WS = X(3)
      E0 = TP*(RJ-1.0)*RJTH
      ES = X(4)*E0
      ET = (1.0-R)*X(1)/DSQRT(R)*TD/T0
      GS = 1.0/TP-2.0*ET/TD*DCOS(WS)
      DN = (GS/(1.0-EP*ES)-1.0/TP)/GN
      CALL STDST
C
C      Complex frequency and coupling strength
C
      CZ = DCMPLX(0.0D0,8.0D0*DATAN(1.0D0)*X(2))
      CE = ET/TD*(1.0-CDEXP(-CZ*TD))
C
C      The complex determinant
C
      CDET = CZ**3+
      *      2.0*(GAMMA+CE*DCOS(WS))*CZ**2+
      *      (OMEGSQ+2.0*(GAMMA+GAMMAN)*CE*DCOS(WS)+CE**2)*CZ+
      *      2.0*GAMMAN*CE**2+
      *      OMEGSQ*DSQRT(1.0+ALPT**2)*CE*DCOS(WS+DATAN(ALPT))
C
      F(1) = DREAL(CDET)
      F(2) = DIMAG(CDET)
      F(3) = WS-(W0*TD-WOT)-ALP*GN*DN*TD/2.0+ET*DSIN(WS)
      F(4) = GS*ES-(RJ-1.0)*RJTH+DN/TS
C
      RETURN
      END
C
      SUBROUTINE STDST
      -----
C
C      Determine steady state parameters of ECLD. The steady state data
are stored in common block ECLDSS.
C
      IMPLICIT REAL*8 (A-H,O-Z)
      COMMON /ECLD/ GN,TP,EP,R,T0,FEXT,TD,ALP,W0,TS,RJTH,RJ,WOT
      COMMON /ECLDSS/ WS,ES,DN,GAMMAN,GAMMAI,GAMMA,OMEGSQ,ALPT
C
C      Damping GAMMAN caused by spontaneous and induced emission
C
      GNP = GN*(1.0-EP*ES)
      GAMMAN = (1.0+GNP*ES*TS)/2.0/TS
C
C      Damping GAMMAI caused by nonlinear gain saturation
C
      EPP = EP/(1.0-EP*ES)
      GS = (1.0-EP*ES)*(GN*DN+1.0/TP)
      GAMMAI = EPP*ES*GS/2.0

```

```

C
C      Decay rate GAMMA of relaxation oscillations of solitary laser
C
C      GAMMA = GAMMAN+GAMMAI
C
C      Square of relaxation oscillation frequency OMEG**2
C
C      OMEGSQ = GNP*GS*ES*(1.0+EPP/GNP/TS)
C
C      (Modified) linewidth enhancement factor.
C
C      ALPT = ALP/(1.0-EP*ES)*(1.0-4.0*GAMMAN*GAMMAI/OMEGSQ)
C
C      RETURN
C      END
C
C      SUBROUTINE START(N,X)
C      -----
C
C      Generate random starting values for X. N is the number of
C      equations.
C
C      IMPLICIT REAL*8 (A-H,O-Z)
C      COMMON /SEARCH/ ISEED,NSF,XF(500,10),PAR(10)
C      DIMENSION X(N)
C
C      Generate a random number between X1L and X1H within which X(1) is
C      expected to lie. RAND is in the range (0,1).
C
C      ISEED = MOD((2**10+3)*ISEED,2**20)
C      RAND = DBLE(ISEED)/2**20
C      X1L = 0.0D+00
C      X1H = 1.0D+00
C      X(1) = (X1H-X1L)*RAND+X1L
C
C      Another random number for X(2).
C
C      ISEED = MOD((2**10+3)*ISEED,2**20)
C      RAND = DBLE(ISEED)/2**20
C      X2L = 1.0D-04
C      X2H = 1.0D-01
C      X(2) = (X2H-X2L)*RAND+X2L
C
C      Another random number for X(3).
C
C      ISEED = MOD((2**10+3)*ISEED,2**20)
C      RAND = DBLE(ISEED)/2**20
C      X3L = -4.0D1*DATAN(1.0D0)
C      X3H = 4.0D1*DATAN(1.0D0)
C      X(3) = (X3H-X3L)*RAND+X3L
C
C      Another random number for X(4).
C
C      ISEED = MOD((2**10+3)*ISEED,2**20)
C      RAND = DBLE(ISEED)/2**20
C      X4L = 0.5D0
C      X4H = 2.5D0
C      X(4) = (X4H-X4L)*RAND+X4L
C
C      RETURN
C      END

```



```

C      SUBROUTINE UPDATE(N,X,INFO)
C      -----
C      Update the library of solutions.
C
C      IMPLICIT REAL*8 (A-H,O-Z)
C      DIMENSION X(N),XOLD(10)
C      COMMON /SEARCH/ ISEED,NSF,XF(500,10),PAR(10)
C
C      Check to see if the current data point already found earlier to
C      within a relative tolerance of 1.0E-07. If so, return.
C
C      OPEN (1,FILE='search_st.out',STATUS='OLD')
C      REWIND 1
10  READ (1,100,END=30) (XOLD(I), I=1,N)
C      DO 20 I = 1,N
C          DIFF = DABS(XOLD(I)-X(I))
C          IF (DIFF.GT.(1.0D-07*DABS(X(I)))) THEN
C              IF (DABS(X(I)).GT.1.0D-10) GO TO 10
C          ENDIF
20  CONTINUE
C      CLOSE (1)
C      RETURN
C
C      30 NSF = NSF+1
C
C      DO 40 I = 1,N
C          XF(NSF,I) = X(I)
40  CONTINUE
C
C      OPEN (1,FILE='search_st.out',STATUS='OLD')
C      WRITE (1,100) (X(I), I=1,N)
C      CLOSE (1)
C
C      100 FORMAT(125E16.8)
C
C      RETURN
C      END
C
C      SUBROUTINE PIKSRT (N,ARR,BRR,CRR,DRR)
C      -----
C      Sorts an array ARR of length N into ascending numerical order, by
C      straight insertion, while making the corresponding rearrangement
C      of
C      the arrays BRR, CRR and DRR.
C
C      IMPLICIT REAL*8 (A-H,O-Z)
C      DIMENSION ARR(N),BRR(N),CRR(N),DRR(N)
C
C      DO 30 J = 2,N
C          A = ARR(J)
C          B = BRR(J)
C          C = CRR(J)
C          D = DRR(J)
C          DO 10 I = J-1,1,-1
C              IF (ARR(I).LE.A) GO TO 20
C              ARR(I+1) = ARR(I)
C              BRR(I+1) = BRR(I)
C              CRR(I+1) = CRR(I)

```

```
      DRR(I+1) = DRR(I)
10    CONTINUE
      I = 0
20    ARR(I+1) = A
      BRR(I+1) = B
      CRR(I+1) = C
      DRR(I+1) = D
30    CONTINUE
C
      RETURN
      END
```

Appendix 4

```

SUBROUTINE FUNC(N,X,ICP,PAR,IJAC,F,DFDU,DFDP)
C -----
C
C      Roots of determinant of linearized rate equations of the external
C      cavity laser diode (ECLD).
C
C      X(1)=SQRT(FEXT), where FEXT is the feedback fraction
C      X(2)=W/2/PI, where W is the (circular) frequency of relaxation
C      oscil.
C      X(3)=WT, where WT is the steady state phase shift in external
C      cavity
C      X(4)=ES/E0, where ES and E0 are the steady state field
C      intensities of
C      the ECLD and the solitary laser, respectively.
C      PAR(1)=TD-TD0, where TD is round trip delay in external cavity
C      in ps,
C      and TD0 is starting delay in ps.
C
C      IMPLICIT REAL*8 (A,B,D-H,O-Z)
C      IMPLICIT COMPLEX*16 (C)
C      DIMENSION X(N),F(N),PAR(*)
C      COMMON /ECLD/ GN,TP,EP,R,T0,FEXT,TD,ALP,W0,TS,RJTH,RJ,WOT,TD0
C      COMMON /ECLDSS/ WS,ES,DN,GAMMAN,GAMMAI,GAMMA,OMEGSQ,ALPT
C
C      PI = 4.0D0*DATAN(1.0D0)
C
C      Update ECLD parameters.
C
C      !      TD = PAR(1)+TD0          !delay in external cavity
C      !      RJ = PAR(1)
C      !      FEXT = X(1)**2          !feedback fraction
C
C      Determine steady state parameters and store in common block ECLDSS
C
C      WS = X(3)
C      E0 = TP*(RJ-1.0)*RJTH
C      ES = X(4)*E0
C      ET = (1.0-R)*X(1)/DSQRT(R)*TD/T0
C      GS = 1.0/TP-2.0*ET/TD*DCOS(WS)
C      DN = (GS/(1.0-EP*ES)-1.0/TP)/GN
C      CALL STDST
C
C      Complex frequency and coupling strength
C
C      CZ = DCMPLX(0.0D0,2.0D0*PI*X(2))
C      CE = ET/TD*(1.0-CDEXP(-CZ*TD))
C
C      The complex determinant
C
C      CDET = CZ**3+
C      *      2.0*(GAMMA+CE*DCOS(WS))*CZ**2+
C      *      (OMEGSQ+2.0*(GAMMA+GAMMAN))*CE*DCOS(WS)+CE**2)*CZ+
C      *      2.0*GAMMAN*CE**2+
C      *      OMEGSQ*DSQRT(1.0+ALPT**2)*CE*DCOS(WS+DATAN(ALPT))
C
C      F(1) = DREAL(CDET)
C      F(2) = DIMAG(CDET)
C      F(3) = WS-(W0*TD-WOT)-ALP*GN*DN*TD/2.0+ET*DSIN(WS)
C      F(4) = GS*ES-(RJ-1.0)*RJTH+DN/TS

```

```

C      RETURN
C      END

C      SUBROUTINE STPNT (NDIM, U, PAR)
C      -----
C
C      Starting conditions.
C
C      IMPLICIT REAL*8 (A-H,O-Z)
C      DIMENSION U(NDIM), PAR(*)
C      COMMON /ECLD/ GN, TP, EP, R, TO, FEXT, TD, ALP, W0, TS, RJTH, RJ, WOT, TD0
C
C      Get ECLD parameters and store in common block ECLD
C
C      CALL GETPAR
C
C      !
C      ! TD0 = TD
C      ! PAR(1) = TD-TD0
C      ! PAR(1) = RJ
C
C      OPEN (1, FILE='search_st.out', STATUS='OLD')
C      READ (1, *) (U(I), I=1, NDIM)
C      CLOSE (1)
C
C      RETURN
C      END

C      SUBROUTINE GETPAR
C      -----
C
C      Get ECLD parameters and store in common block ECLD.
C
C      IMPLICIT REAL*8 (A-H,O-Z)
C      COMMON /ECLD/ GN, TP, EP, R, TO, FEXT, TD, ALP, W0, TS, RJTH, RJ, WOT, TD0
C
C      OPEN (1, FILE='ecl.d.in', STATUS='OLD')
C      READ (1, *) GN !gain coefficient (8.1E-19 cm**3/ps)
C      READ (1, *) TP !photon lifetime (2 ps)
C      READ (1, *) EP !nonlinear gain coefficient (9.0E-18 cm**3)
C      READ (1, *) R !laser facet reflectivity (0.31)
C      READ (1, *) TO !solitary laser cavity round trip time (8 ps)
C      READ (1, *) FEXT !feedback fraction (1.0E-04)
C      READ (1, *) TD !delay in external cavity (20ps for 3mm EC)
C      READ (1, *) ALP !linewidth enhancement factor (6)
C      READ (1, *) W0 !freq of solitary laser (1.45E+15 rad/s for
WL=1300 nm)
C      READ (1, *) TS !carrier lifetime (2ns)
C      READ (1, *) RJTH !current density at threshold (8.55E+14 cm**3/ps)
C      READ (1, *) RJ !current density relative to threshold (1.2)
C      CLOSE (1)
C
C      WOT = W0*TD-DMOD(W0*TD, 8.0D0*DATAN(1.0D0))
C      FEXT = FEXT**2
C
C      RETURN
C      END

C      SUBROUTINE STDST
C      -----
C

```

```

C      Determine steady state parameters of ECLD. The steady state data
are
C      stored in common block ECLDSS.
C
      IMPLICIT REAL*8 (A-H,O-Z)
      COMMON /ECLD/ GN,TP,EP,R,T0,FEXT,TD,ALP,W0,TS,RJTH,RJ,W0T,TD0
      COMMON /ECLDSS/ WS,ES,DN,GAMMAN,GAMMAI,GAMMA,OMEGSQ,ALPT
C
C      Damping GAMMAN caused by spontaneous and induced emission
C
      GNP = GN*(1.0-EP*ES)
      GAMMAN = (1.0+GNP*ES*TS)/2.0/TS
C
C      Damping GAMMAI caused by nonlinear gain saturation
C
      EPP = EP/(1.0-EP*ES)
      GS = (1.0-EP*ES)*(GN*DN+1.0/TP)
      GAMMAI = EPP*ES*GS/2.0
C
C      Decay rate GAMMA of relaxation oscillations of solitary laser
C
      GAMMA = GAMMAN+GAMMAI
C
C      Square of relaxation oscillation frequency OMEG**2
C
      OMEGSQ = GNP*GS*ES*(1.0+EPP/GNP/TS)
C
C      (Modified) linewidth enhancement factor.
C
      ALPT = ALP/(1.0-EP*ES)*(1.0-4.0*GAMMAN*GAMMAI/OMEGSQ)
C
      RETURN
      END
C
      SUBROUTINE BCND
      -----
C
C      Dummy routine
C
      RETURN
      END
C
      SUBROUTINE ICND
      -----
C
C      Dummy routine
C
      RETURN
      END
C
      SUBROUTINE FOPT
      -----
C
C      Dummy routine
C
      RETURN
      END

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REPORT DOCUMENTATION PAGE

Form Approved
OMB No. 0704-0188

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1. AGENCY USE ONLY (Leave Blank)		2. REPORT DATE 10/24/97		3. REPORT TYPE AND DATES COVERED FINAL 5/1/96-7/30/97	
4. TITLE AND SUBTITLE An Investigation of Deterministic and Stochastic Properties of Microwave/Millimeter Wave Signals Generated in Laser Diodes with Short External Cavity				5. FUNDING NUMBERS N00014-96-1-0794	
6. AUTHORS Guifang Li					
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) Rochester Institute of Technology One Lomb Memorial Drive rochester, NY 14623				8. PERFORMING ORGANIZATION REPORT NUMBER	
9. SPONSORING / MONITORING AGENCY NAME(S) AND ADDRESS(ES) Office of Naval Research Ballston Centre Tower One 800 North Quincy Street Arlington, Va 22217-5660				10. SPONSORING / MONITORING AGENCY REPORT NUMBER	
11. SUPPLEMENTARY NOTES					
12a. DISTRIBUTION / AVAILABILITY STATEMENT APPROVED FOR PUBLIC RELEASE				12b. DISTRIBUTION CODE	
13. ABSTRACT (Maximum 200 words) The underlying mechanism of the high-frequency intensity oscillations in laser diodes with short external cavity has been determined. From a nonlinear dynamic point of view, Hopf bifurcation is responsible for the occurrence of the high-frequency intensity oscillations. However, Hopf bifurcation is only the necessary condition. The necessary and sufficient conditions are that Hopf bifurcation occurs and the limiting point of existence of a higher-order mode is above the stability boundary of a lower-order mode. The noise characteristics of the high-frequency oscillations can be measured using the HP 3048A phase and amplitude noise measurement system.					
14. SUBJECT TERMS Laser Diodes, Optical Communications, Nonlinear Dynamics Subcarrier Multiplexing				15. NUMBER OF PAGES 37	
				16. PRICE CODE	
17. SECURITY CLASSIFICATION OF REPORT	18. SECURITY CLASSIFICATION OF THIS PAGE	19. SECURITY CLASSIFICATION OF ABSTRACT		20. LIMITATION OF ABSTRACT	